

The Rotorcraft Aerodynamics Library:

A Modelica Library for Simulation of Rotorcraft Aerodynamics and Whirl Flutter



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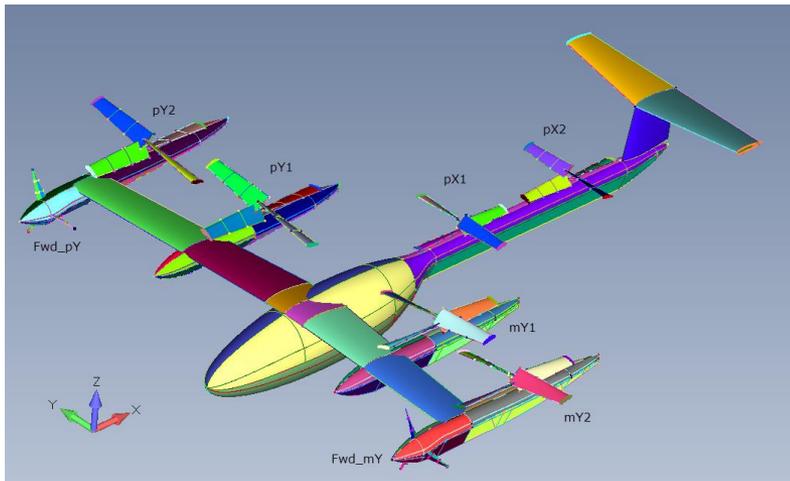
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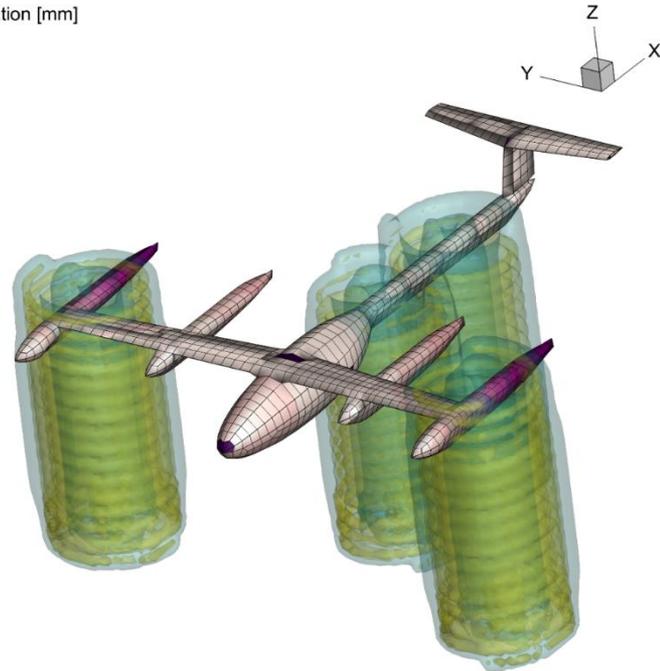
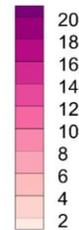
Increasing Need for Multidisciplinary Rotorcraft Modeling

- Emerging eVTOL (electric Vertical Take-Off and Landing) aircraft tightly couple many physical domains
 - Aerodynamics, rotor mechanics+dynamics, electrical motor dynamics, control system, power electronics, etc.
 - Many independent rotors for vertical lift and forward propulsion



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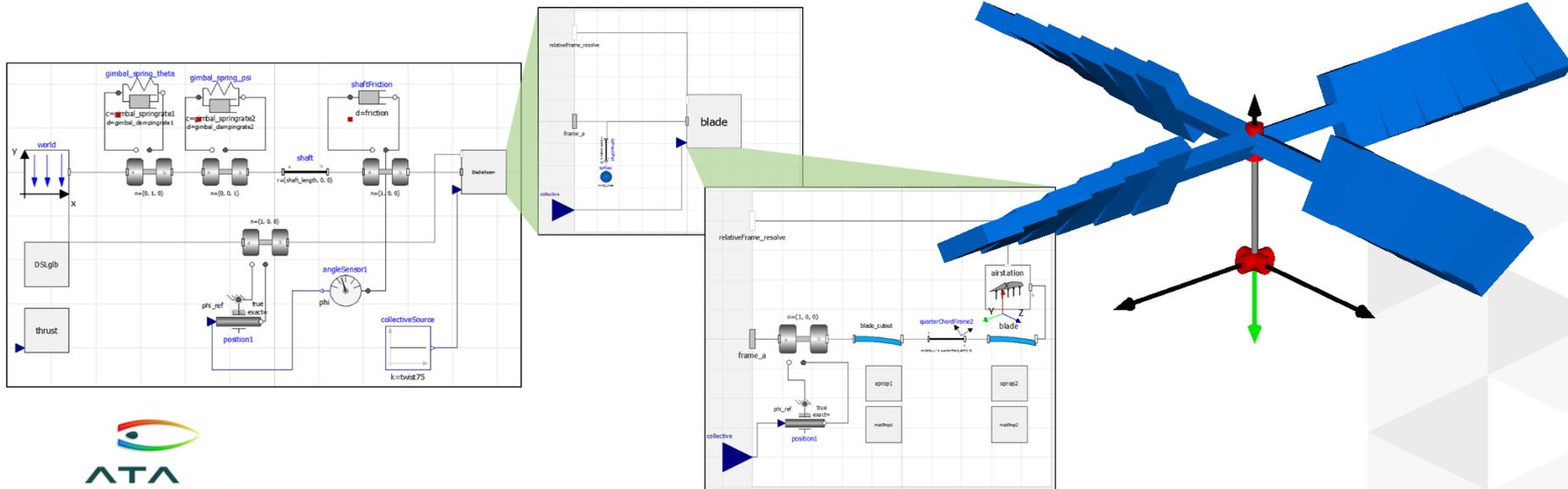


What Makes the eVTOL Problem Difficult?

- Multiple interacting rotor wakes
 - Traditional rotorcraft have few, widely spaced rotors
- Variable RPM rotors
 - Most rotorcraft are designed for a constant RPM
 - Many reasons: engine constraints/power optimization, avoiding structural modes, simplifying envelope calculations (e.g., whirl flutter)
- Electric rotors
 - Coupling with electric system requires power supply, thermal, and efficiency considerations
- Independent rotors
 - Under-constrained rotor trim problem (more rotors than trim objectives)
- Existing analysis tools are insufficient
 - Designed for aero-structural analysis of traditional rotorcraft (few rotors at fixed RPM)
 - Cannot analyze coupled electrical system or variable RPM

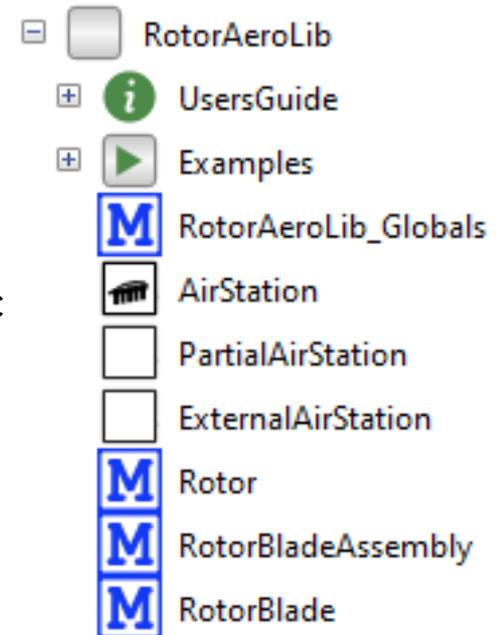
Modelica Enables Easy Coupling of the Various Physical Domains

- Many components can already be modeled/coupled with the MSL
 - Multibody dynamics and rotor mechanics
 - Unique mechanisms can be modeled
 - Various hub topologies and control mechanisms
 - Electric motors and electric power systems
 - Aircraft guidance and control system
- Aerodynamics need to be separately modeled and coupled to the blades



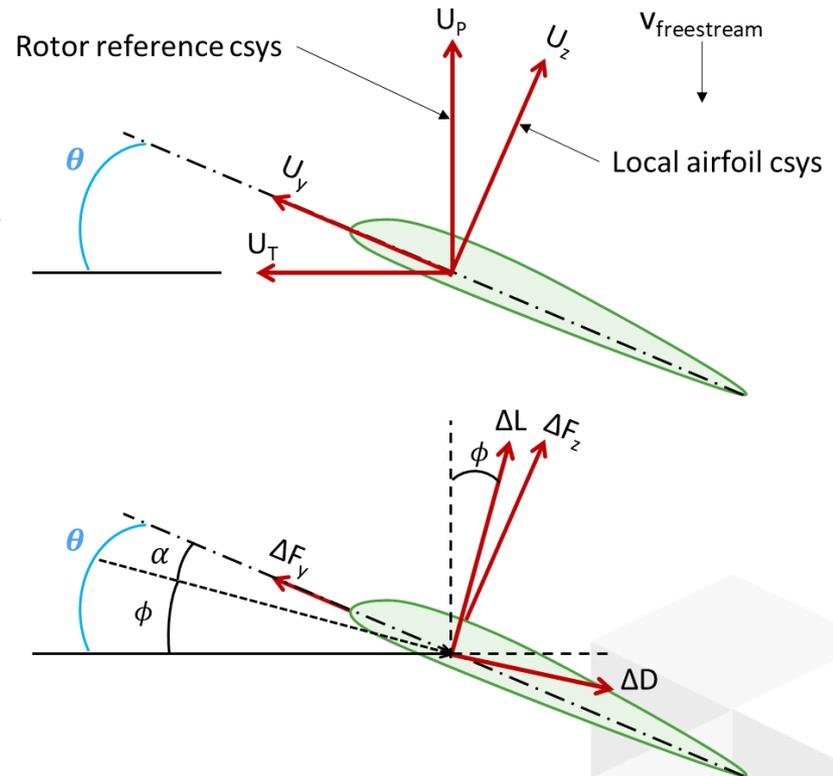
The Rotorcraft Aerodynamics Library (RotorAeroLib)

- Supports modeling rotor aerodynamics within a Modelica model
- Compliments the MultiBody library of the Modelica Standard Library
- Contains specialized modeling blocks for:
 - Modeling blade aerodynamics and transferring forces to blade
 - Modeling the rigid or flexible blade with twist and cross-sectional mechanical/aerodynamic properties
 - Assembling multiple blades into a rotor
 - Interfacing the blades with the rotor control system (i.e., swashplate and linkages)
- Makes use of open-source *DeployStructLib* Modelica library for rigid/flexible blades
- Usage examples included



Blade Aerodynamics Start with Blade Element Theory (BET)

- *RotorAeroLib.AirStation* model calculates the blade aerodynamic forces
- An *AirStation* is attached in the airfoil coordinate system
- Also connects to the rotor reference coordinate system to define geometric/collective angle
- Multiple *AirStations* span the length of the blade to capture varying air flow speeds
 - Ultimately converging on the asymptotic limit
- Lift coefficients defined as a quadratic function of α
- Most of this merely sets up basic fluidic force calculations and projects the forces into the correct coordinate system



θ = *geometric/collective angle*
 α = *angle of attack*
 ϕ = *inflow angle*

Advanced Options Implement Blade Element Momentum Theory (BEMT) and Other Corrections

- Global parameters in *RotorAeroLib*. *RotorAeroLib_Globals* enable advanced correction factors:

Inflow correction for BEMT:

$$\lambda^2 + \left(\frac{\sigma C_{l,\alpha}}{8} - \lambda_c\right) \lambda - \frac{\sigma C_{l,\alpha}}{8} \theta_{\tilde{r}} = 0$$

$$U_P = V_r + \lambda V_{tip}$$

Aspect ratio correction:

$$A_R = 0.75 \frac{R}{c} \quad F_{AR} = \frac{A_R}{A_R + 2}$$

Mach number correction:

$$M = \frac{U}{c_s} \quad F_M = \frac{1}{\sqrt{1 - M^2}}$$

Tip loss correction:

$$F_{tiploss} = \tanh\left(\frac{1 - \frac{r}{R}}{1 - \mu}\right)$$

Unsteady aerodynamics:

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -0.01375 \left(\frac{2U}{c}\right)^2 & -0.3455 \left(\frac{2U}{c}\right) \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} \alpha(t)$$

$$C_i(t) = C_{l,\alpha} \begin{bmatrix} 0.006825 \left(\frac{2U}{c}\right)^2 & 0.10805 \left(\frac{2U}{c}\right) \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \frac{C_{l,\alpha}}{4} \alpha(t)$$

Noncirculatory unsteady aerodynamics:

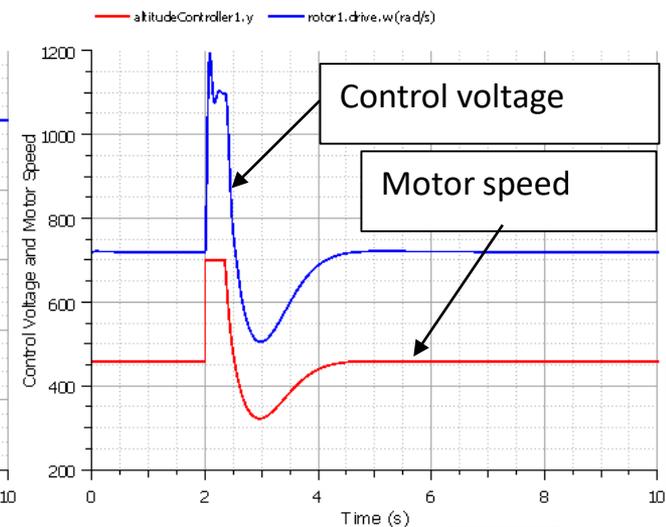
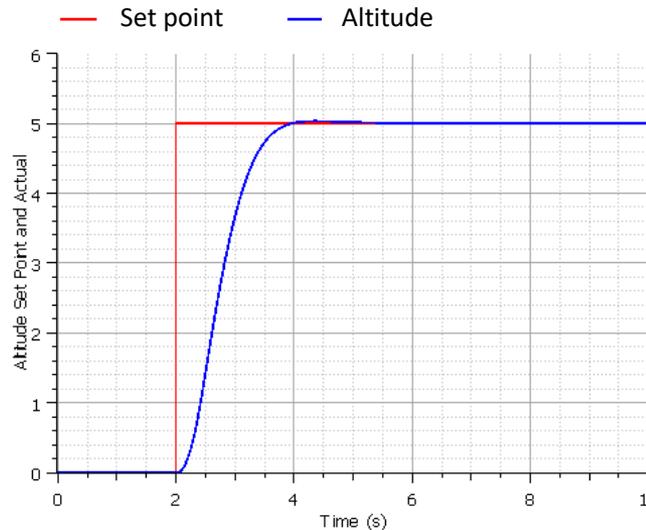
$$C_{l,nc} = \pi b \left(\frac{\dot{\theta}}{U} + \frac{\ddot{h}}{U^2} - \frac{ba\ddot{\theta}}{U^2} \right)$$

- Inflow correction affects the inflow airspeed U_P
- The unsteady aero terms change the coefficient of lift C_l
- The others are factors on the blade lift ΔL
- Some of these terms may significantly increase computational cost

Quadcopter Example

- Couples rotordynamics, multibody dynamics, lifting line aerodynamics, motor electro-dynamics
 - Rigid rotors with all but unsteady aerodynamic correction factors
 - Motors are individually voltage-controlled
 - Constrained max motor speed
- Model starts in hover with rotors spun up to counter gravity

Altitude set point starts at zero then steps to 5 m



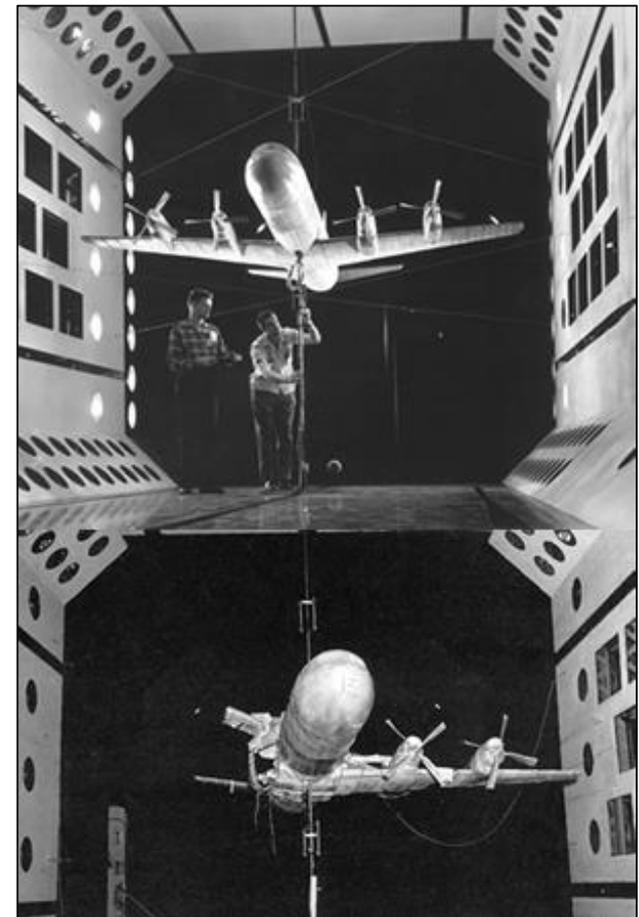
Analysis of Aircraft Whirl Flutter

- Aeroelastic instability caused by the interaction of the aircraft structural dynamics, rotor gyroscopic forces, and rotor aerodynamics
- Initial studies performed in the 60's
 - Houbolt and Reed, Bland and Bennet
 - Driven by early aircraft crashes of Lockheed Electra
 - Interest today in tiltrotor and other non-conventional aircraft
- Directly impacts the aircraft flight envelope



Credit: NASA

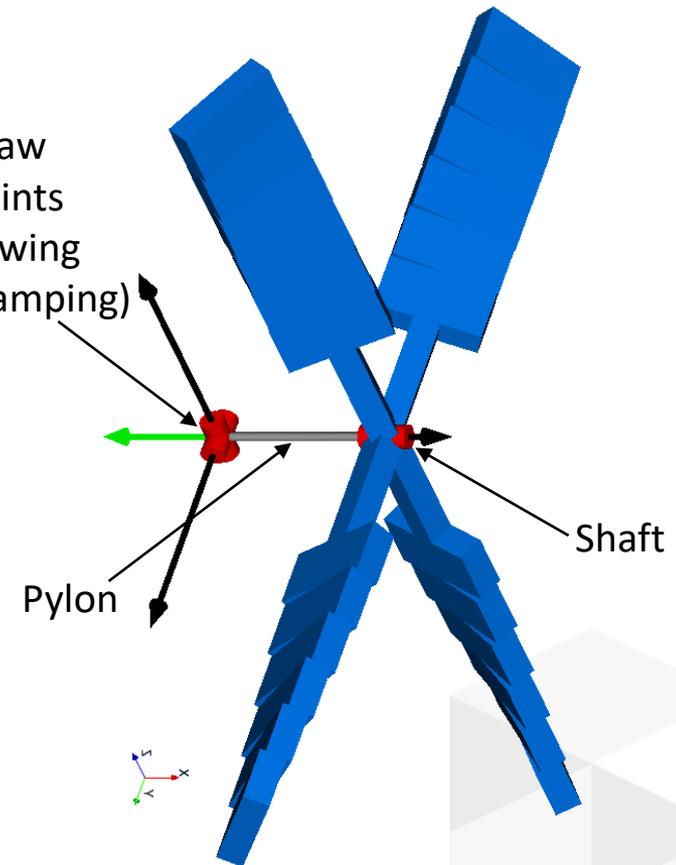
<https://www.youtube.com/watch?v=j6Q5ggtV-y8>



Bland and Bennett Propeller Model Use for Whirl Flutter Analysis

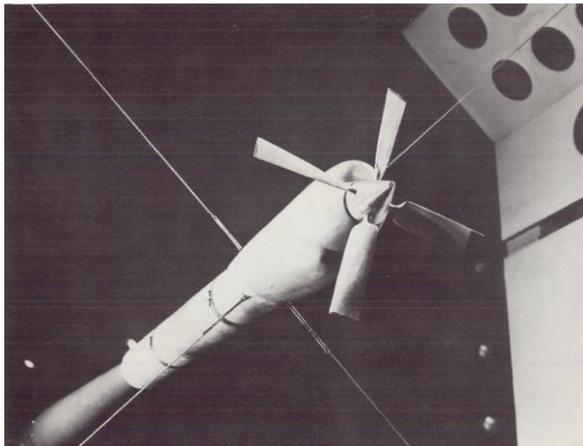
- Modelica model of Bland and Bennett propeller
 - Linearized blade twist
 - Lift-curve slope 5.7/rad
 - Unsteady aerodynamic effects included
 - No in-plane drag
 - 6 airstations per blade
 - Additional airstations showed minimal change in results
- Goal is to find the flutter boundary

Pitch and yaw stiffened joints (represent wing stiffness/damping)

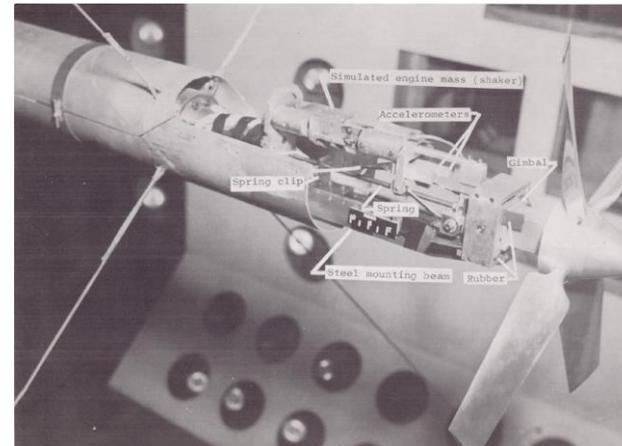


Bland and Bennett Validation Data

- Wind-tunnel whirl flutter measurements taken by Bland and Bennett in 1963 at NASA LaRC Transonic Dynamics Tunnel
- Flutter boundary was determined for various blade pitch angles (β) in a parameter space of reduced velocity/required damping for stability



Source: Bland and Bennett
S.R. Bland and Bennett, R.M., "Wind-Tunnel Measurement of Propeller Whirl-Flutter Speeds and Static-Stability Derivatives and Comparison with Theory", NASA TN D-1807, 1963.



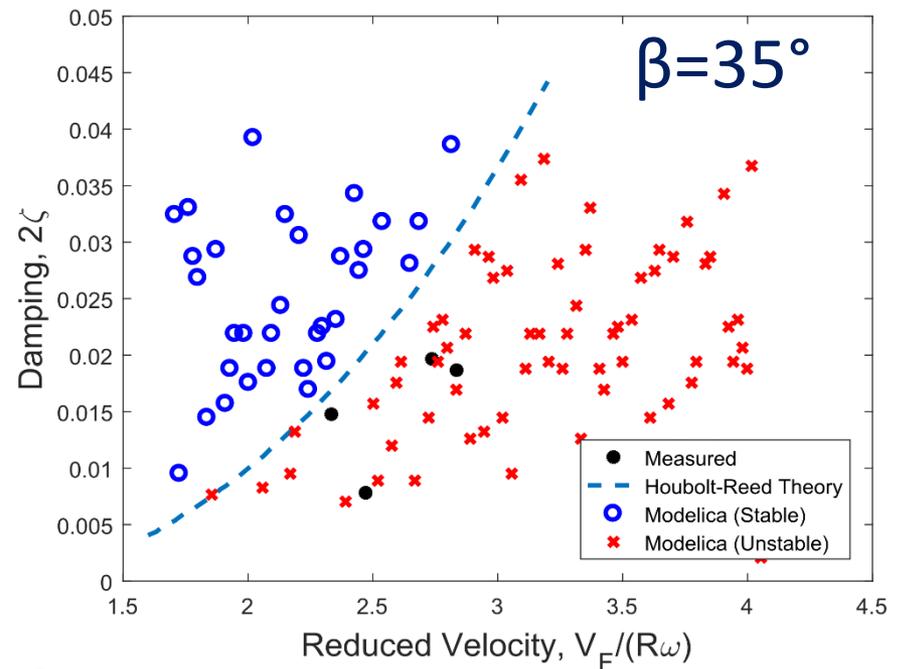
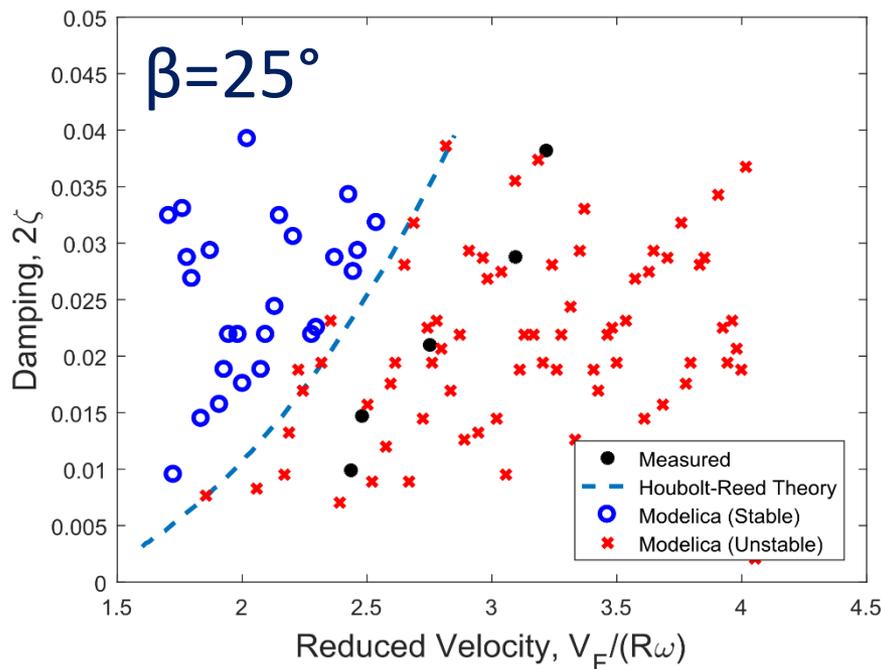
Source: Bland and Bennett

Verification and Validation – Stability Calculations

- Modelica model is solved with the rotor speed and aerodynamic forces balanced at initialization
 - Linearized system extracted at $t=0$ sec
- Eigenvalues of linearized system extracted to obtain frequency and damping at an operating point
 - Unstable System (positive real part): **X**
 - Stable System (negative real part): **O**
- Parametric study explored stability within the parameter space of reduced velocity and structural damping
 - Varied damping of springs at base of pylon (i.e., effective wing modal damping) and freestream velocity
 - Performed for a range of fixed blade collectives

Whirl Flutter Stability Boundaries (1/2)

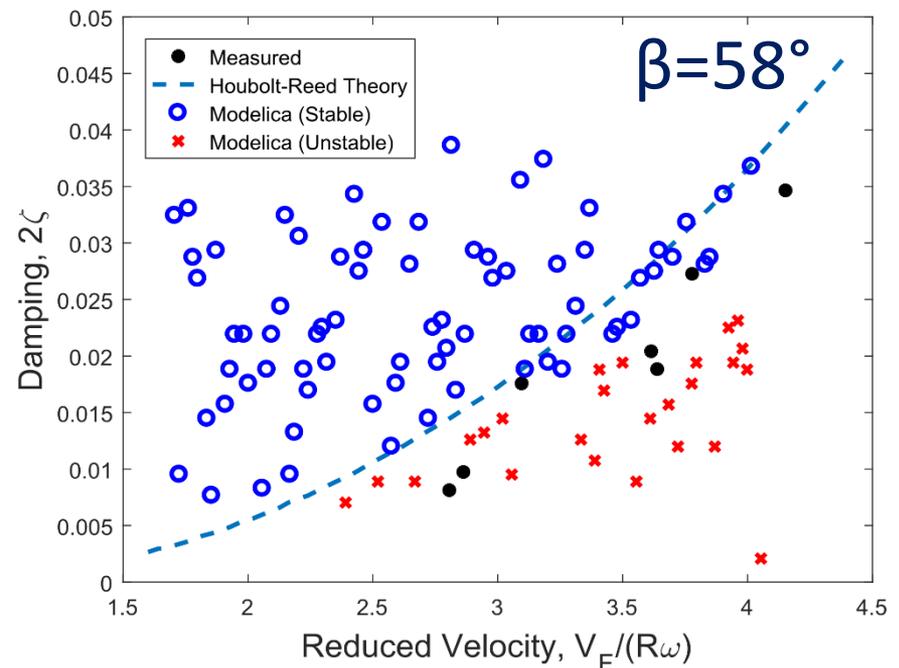
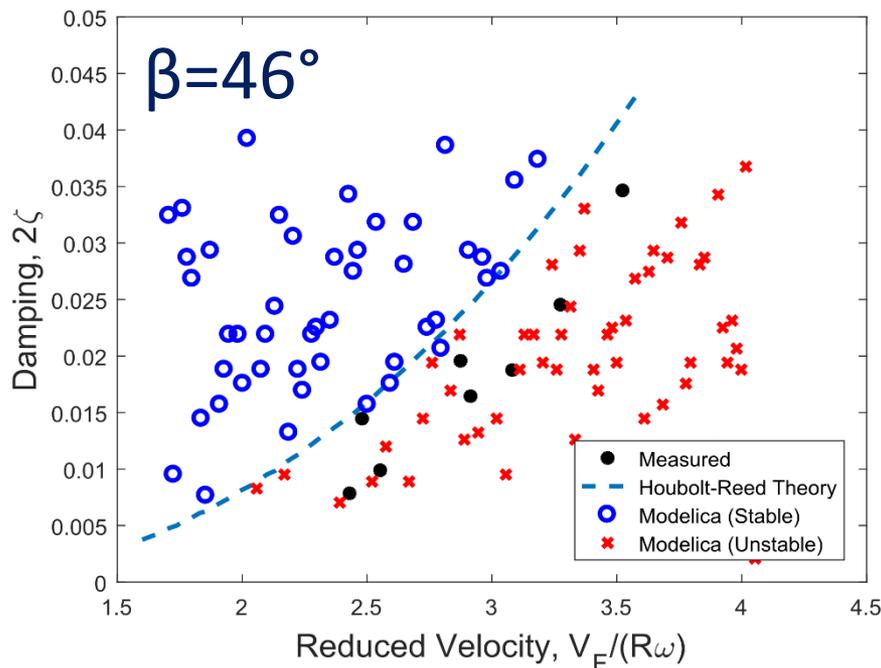
- Modelica whirl flutter boundary compared to an analytical Houbolt-Reed formulation and measured stability boundary data
- Predictions show good agreement with experimental data and between analysis types despite different formulations



Unstable System: X
Stable System: O

Whirl Flutter Stability Boundaries (2/2)

- At increased blade pitch angles, the Modelica predictions move closer to the experimental results than the analytical boundary
- Reduced conservatism



Unstable System: ✖

Stable System: ○

Conclusions

- *RotorAeroLib* enables wide ranging design studies of complex multiphysics phenomena for rotorcraft
- Available on GitHub
 - <https://github.com/ATAEngineering/RotorAeroLib>
- Developed using OpenModelica
 - Help ensuring compatibility with other compilers would be much appreciated
 - Bug reports and suggestions are always welcome



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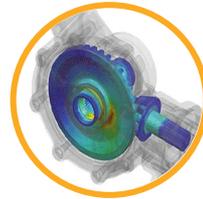
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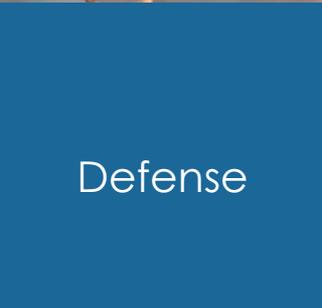
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